Polymer Composites with Hollow Glass Microspheres: Processing, Properties and Applications

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> > November 6, 2012



Outline

Overview of 3M[™] Glass Bubbles

- Physical Properties of Hollow Glass Microspheres (HGM)
- Composition, Strength, Density and Particle Size

Formulating with Hollow Glass Microspheres

Polymer Processing with Hollow Glass Microspheres

- Compounding, Extrusion
- Injection Molding

Benefits of Hollow Glass Microspheres

- Material
- Processing

Application Examples



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3M[™] Glass Bubbles Overview



3M[™] Glass Bubbles

Property	Value
Shape	Hollow, thin walled, unicellular spheres
Composition	Soda-lime borosilicate glass
Color	White
True Density [†]	0.12 - 0.60 g/cc
Crush Strength*	250 – 28,000 psi
Hardness	Mohs scale 5
Softening Temp	600° C
Size	15 - 65 microns <

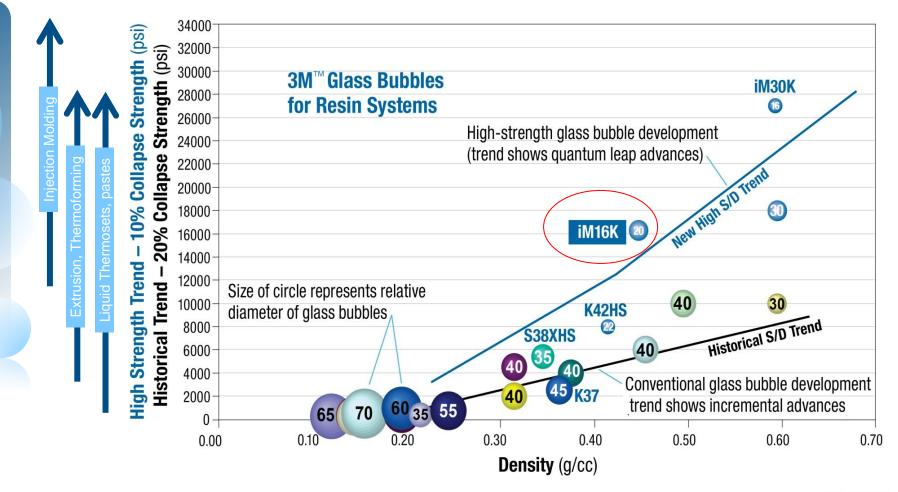
•ASTM D 3102-78 Standard Practice for the Determination of Isostatic Collapse Strength of Hollow Glass Microspheres (withdrawn in May 1984)

[†]Helium Gas Pycnometer



Wall thickness

3M[™] Glass Bubbles Isostatic Collapse Strength



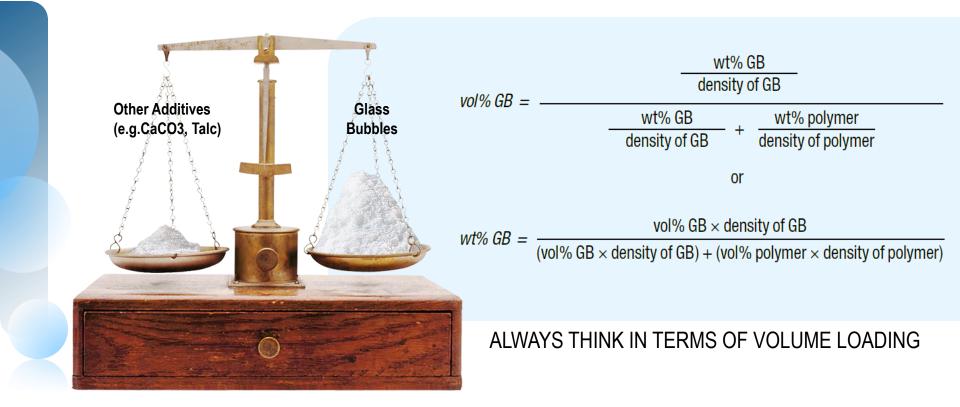


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Formulating with HOIOW Glass Microspheres

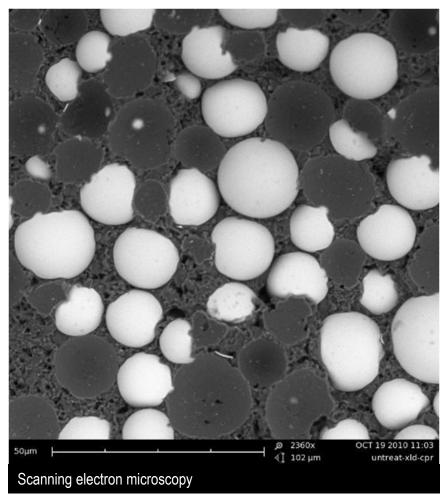


Formulating with GBs on Volume Basis





Maximum practical GB loading



Component	Density	Weight	Volume	
	g/cc	%	%	
PP	0.9000	64.000	54.237	
GB	0.6000	36.00	45.76	
_	0.7627 Domoitu	100.000	100.000	
Totals Component	Density	Weight	Volume	
Component	Density g/cc	Weight %	Volume %	
_	Density	Weight	Volume	

Component	Density g/cc	Weight %	Volume %
PVC	1.4000	74.000	54.950
GB	0.6000	26.00	45.05
Totals	1.0396	100.000	100.000
Component	Density	Weight %	Volume %
	q/cc	/0	/0
PVC	g/cc 1.4000	78.500	7 0 54.539
PVC GB			

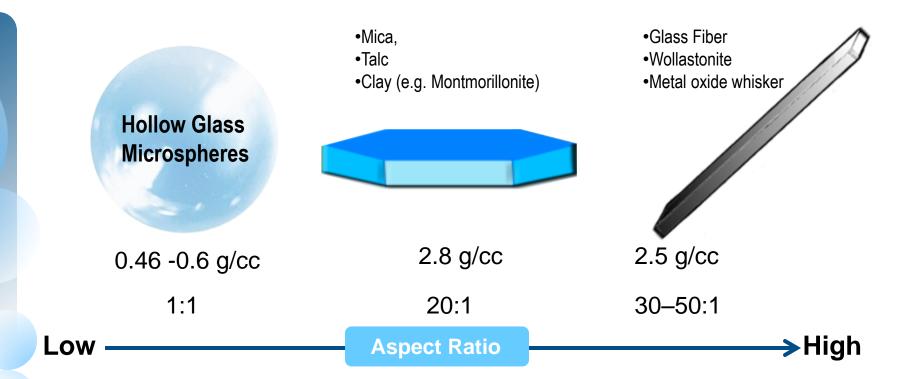


Formulating with GBs- TPOs

		Function
Polymer Phase	PP (Polypropylene) homo, co, high crystallinity) PE (polyethylene)	Main Matrix
Elastomer Phase	EPR (Ethylene propylene rubber) EPDM (EP-diene rubber) EO (ethylene-octene), EB (ethylene-butadiene) SEBS (Styrene-ethylene-butadiene-styrene)	Improve cold temperature impact properties
Reinforcing Filler Phase	Talc, Nano Clay, Mica Glass fiber (Short, Long), wollastonite, whiskers, ceramic fibers	Increase stiffness (strength, modulus), HDT
Additives	Pigments, Stabilizers	UV, Heat, etc



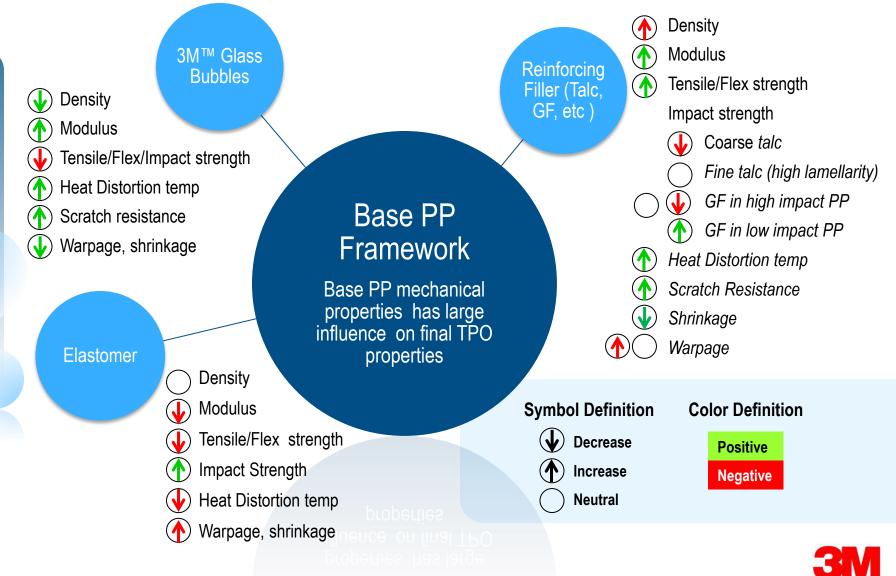
Comparison of 3M[™] Glass Bubbles to typical fillers used in TPOS



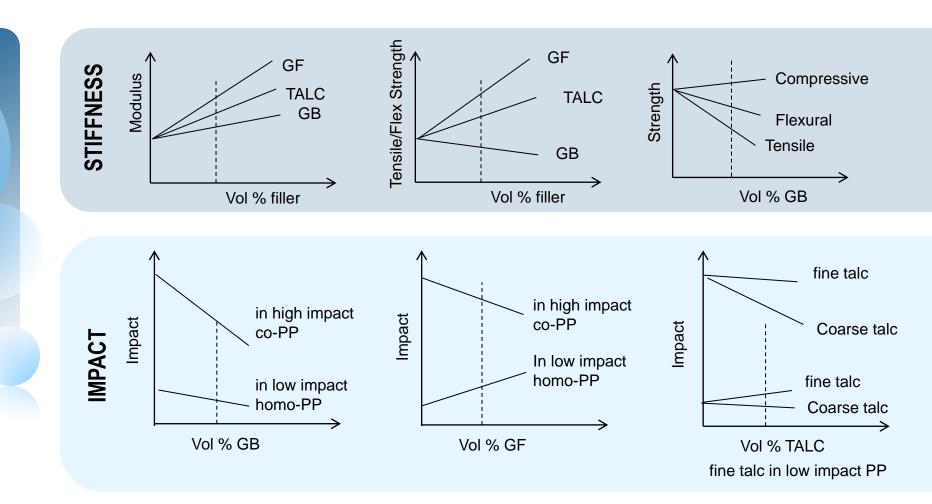
Due to the differences in density, size and aspect ratio, glass bubble containing recipes need to be carefully formulated to maintain a good balance of mechanical properties while reducing density



Effect of Major Components on TPO Properties

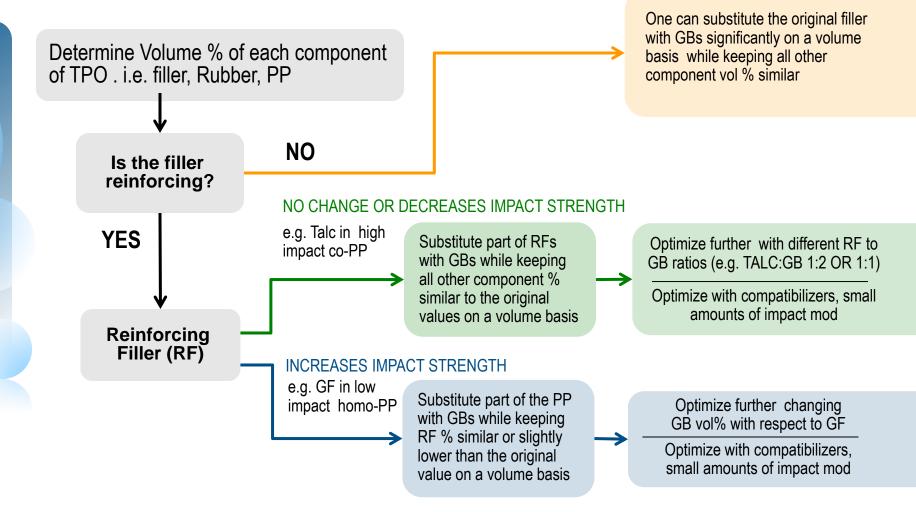


Extent of Individual Contribution of Fillers to Stiffness and Impact





Glass Bubble Formulation Strategy in the Presence of Other Fillers



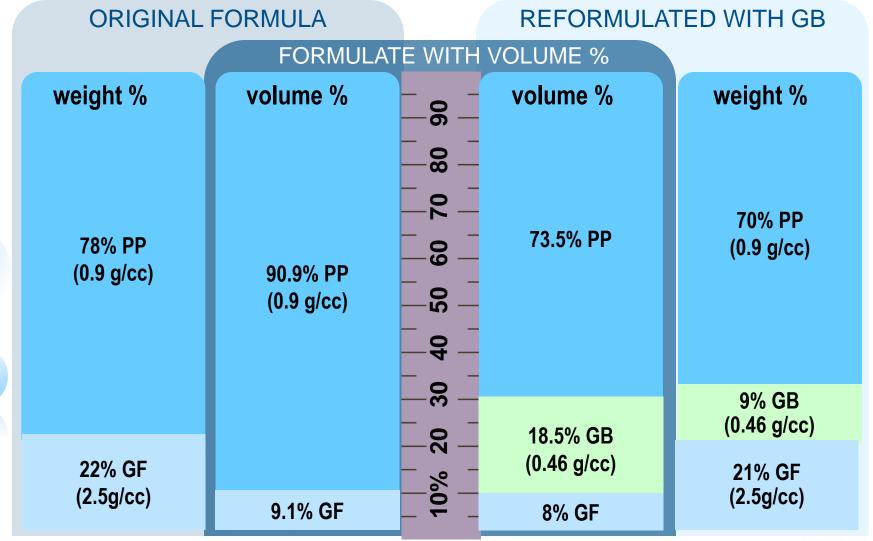


Formulation Scheme in the Presence of Talc

ORIGINAL	FORMULA		REFORMULATED WITH GB		
	FORMULA	TE WITH	VOLUME %		
weight %	volume %	0	volume %	weight %	
60% PP (0.9 g/cc)	70% PP	40 50 60 70 80	70% PP	68.5% PP (0.9 g/cc)	
20% RUBBER (0.87 g/cc)		 30		22% RUBBER	
20% TALC	23% RUBBER	0% 20 - -	23% RUBBER	(0.87 g/cc)	
(2.78 g/cc)	7% TALC	- 7 -	5% GB 2% TALC	7% TALC (2.78 g/cc) 2.5% GB (0.46 g/cc)	



Formulation Scheme in the Presence of GF in a Low Impact PP





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Technical Data HOIIOW Glass Microspheres

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Component	Form	nula 1	Form	Formula 2		Formula 3		ula 4	Formula 5	
	Р	P	PP-GB10		PP-GB10-mapp		PP-GB20		PP-GB20-mapp	
	Wt%	Vol%	Wt%	Vol%	Wt%	Vol%	Wt%	Vol%	Wt%	Vol%
PP homopolymer	100	100	90	83	87	80.60	81	69	76	65.84
GB-iM16K			10	17	10	16.65	19	31	20	30.78
Mapp compatibilizer					3	2.75			4	3.38
Final	100	100	100	100	100	100	100	100	100	100
Density	0	.9	0.835		0.835		0.785		0.785	
Tensile Strength @ RT (Mpa)	30).2	22.3		29.8		16.2		31.0	
Tensile Strength @ 90°C(Mpa)	1().1	8.6		11.6		7.7		13.5	
Tensile Modulus @RT (Mpa)	11	95	1670		1513		1974		1830	
Tensile Modulus @ 90°C (Mpa)	1	62	230		230		340		300	
Flexural Strength (Mpa)	37.9		36	6.6	44.3		32.5		49.2	
Flexural Modulus @1 % secant (Mpa)	10	63.	1410		1486		1585		1740	
Izod impact Strength at RT (J/m)	38	3.5	24	1.2	34	l.8	20	.9	30.3	



Impact Strength in Unfilled PP Copolymer

ASTM D256 Izod Pendulum impact strength –Test Method A- Notched (kj/m ²)	As Received Unfilled	Part with IM16K	Part with iM16K
Density g/cc	0.9	0.86	0.83
Borealis Standard PP (Homopolymer H503)	4.54	4.16	3.36
Borealis Copolymer (CP284)	19.16	7.8	5.4



Industrial Business Group Homopolymer PP based TPOs Containing Talc Partial Replacement

Component	Formula 1		Formula 2		Formula 3		Formula 4		
	PP-	PP-T20		PP-T10 GB4		PP-T10 GB4 -mapp		20-mapp	
	Wt%	Vol%	Wt%	Vol%	Wt%	Vol%	Wt%	Vol%	
PP homopolymer	80	92.5	86	88.6	83	85.5	77	65.84	
GB-iM16K			4	8	4	8	20	30.78	
Talc	20	7.5	10	3.4	10	3.4			
Mapp compatibilizer					3	3.1	4	3.38	
Final	100	100	100	100	100	100	100	100	
Density	(1.0	046	0.942		0.943		0.785		
Tensile Strength @ RT (MPa)	31	1.7	27.0		32.7		31.0		
Tensile Strength @ 90 °C (MPa)	12	2.5	11	.4	13.5		13.5		
Tensile Elongation (%)	1	0	40		12		6		
Tensile Modulus@ RT (MPa)	21	10	1900		1835		1830		
Tensile Modulus@ 90 °C (MPa)	27	70	20	265		250		300	
Flexural Strength (MPa)	4	9	45		50		49.2		
Flexural Modulus @1 % secant (MPa)	16	50	1620		1620		1740		
Izod impact Strength at RT (J/m) © 3M 2012. All Rights Reserved.	3	32	28		39		30.3		

Industrial Business Group High Impact Ductile TPOs Containing Talc Partial Replacement

Component	Formula 1		Form	nula 2	Formula 3	
	Wt%	Vol%	Wt%	Vol%	Wt%	Vol%
High Impact PP containing rubber	100	100	80	92.74	87.68	91.92
Talc			20	7.26	9.41	3.20
iM16K-GB					2.91	4.88
Final	100	100	100	100	100	100
Density	0.8	377	1.021		0.926	
Tensile Strength (Mpa)	17	7.2	18.8		16.8	
Flexural Strength (Mpa)	26	5.9	33.1		29.7	
Flexural Modulus (Mpa)	915		1585		1310	
Izod impact Strength at RT (J/m)	72	25	64	45	430	



PP Containing Glass Fibers

Component	Form	iula 1	Formula 2		
	-	ection Molding htrol	Standard Injection Molding PP/GF/GB		
	Wt%	Vol%	Wt%	Vol%	
HC- PP	78	91	68.2	70.14	
GF	22	9	19.2	7.12	
iM16K-GB			9.96	20.06	
Compatibilizer			2.64	2.68	
Final	100	100	100	100	
Density	1.()46	0.9)27	
Tensile Modulus (Mpa)	40	50	39	60	
Flexural Strength (Mpa)	1(00	94		
Flexural Modulus @1 % secant (Mpa)	26	06	3020		
Izod impact Strength at RT (J/m)	54	1.5	51.8		



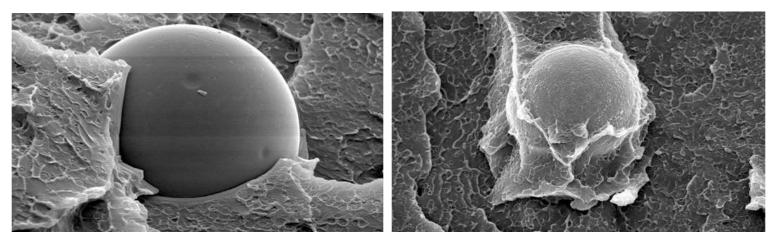
Nylon 66 with 30wt.% Glass Fiber Comparison of Glass Bubble Containing Systems

Component.	Formula 1		Formula 2		Formula 3	
	PA 6,6 Base Resin + 30w% Glass Fiber		PA 6,6 Base Resin + 30w% Glass Fiber + 5w% iM16K		PA 6,6 Base Resin 30w% Glass Fiber 10w% iM16K	
	Wt%	vol%	Wt%	vol%	Wt%	vol%
PA 6,6	70	83.9	65	71.4	60	60.8
Glass Fiber	30	16.1	30	14.7	30	13.6
iM30K-GB						
iM16K-GB			5	13.9	10	25.6
GB/GF VOL RATIO			0.94		1.9	
Final %	1	00	100	100	100	100
Vol.% Glass	16	6.1	28.6		39.2	
Density	1.	37	1.25		1.15	
Tensile Strength (MPa)	19	1.4	176.9		164.1	
Tensile Elong. (%)	6	.6	6.3		5.4	
Tensile Modulus (MPa)	4454		4434		4595	
Flexural Modulus (MPa)	74	70	7598		8044	
RT Izod impact Strength (kJ/m2)	8	.9	8.6		7.7	



Silane Treated GBs

FOR FURTHER COMPATIBILITY WITH VARIOUS RESINS, SILANE TREATED GLASS BUBBLES ARE AVAILABLE



Untreated Bubble

Treated Bubble



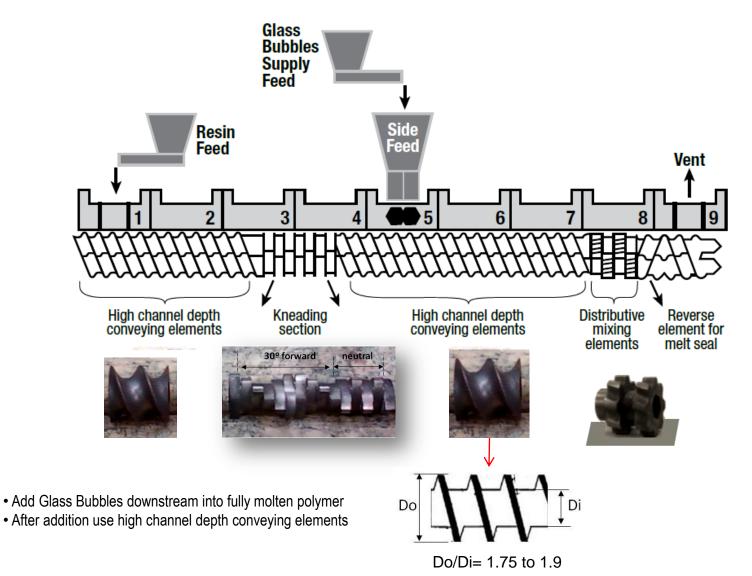
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Polymer Processing with 3M[™] Glass Bubbles

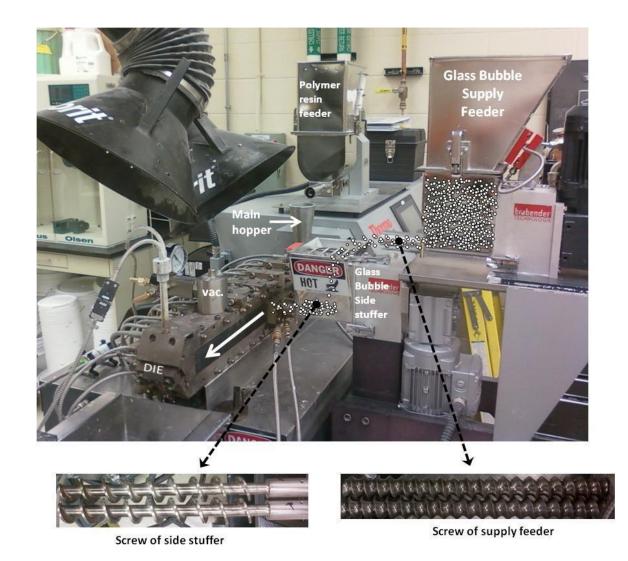


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Incorporation of 3M[™] Glass Bubbles via Twin Screw Extrusion

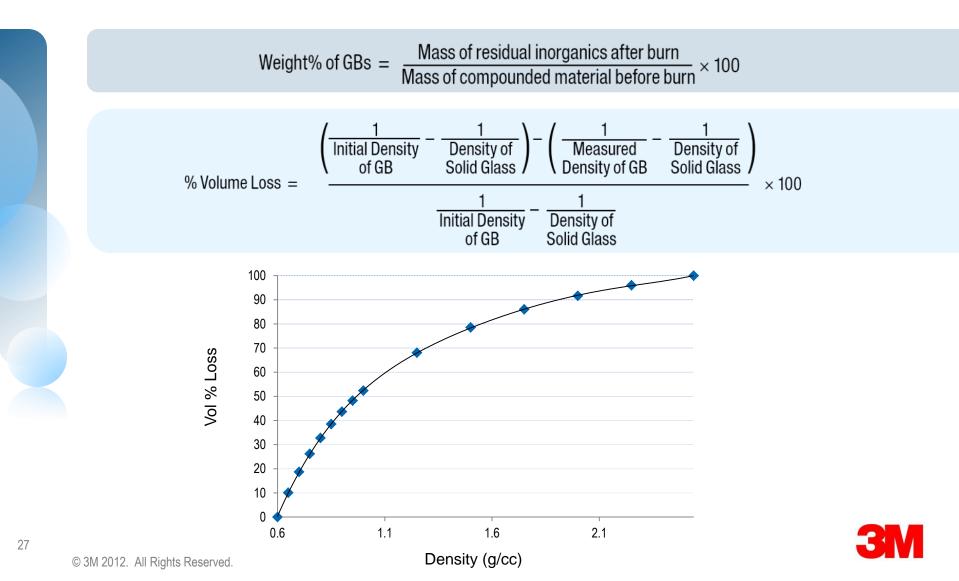








Determining Glass Bubble Concentration and Survival Rate

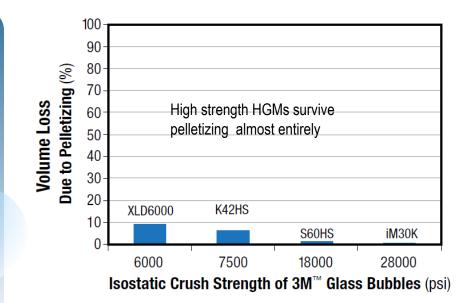


Parameters that are Influential in GB Survival During Compounding

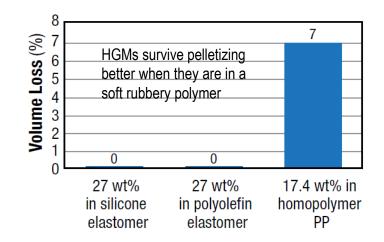
- Pelletizing
- Polymer Viscosity
- HGM Loading –Fill Ratio
- Back Pressure
- Channel Depth in the screw channels



Parameters that are influential in HGM Survival During Compounding -Effect of Pelletizing



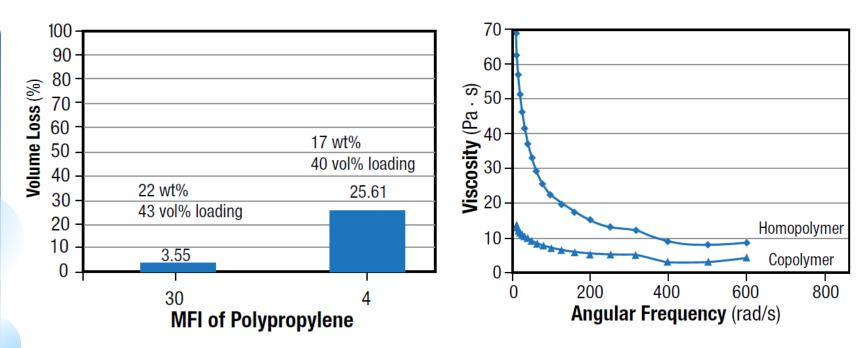
% HGM volume loss due to pelletizing as a function of isostatic crush strength - in homopolymer polypropylene with an MFI of 4 g/10 min at 230°C, 2.16 kg



% Glass bubble volume loss due to pelletizing as a function of resin system used. In elastomeric soft resins, glass bubble survival is higher during pelletizing (glass bubble with 6000 psi crush strength, 0.3 g/cc)



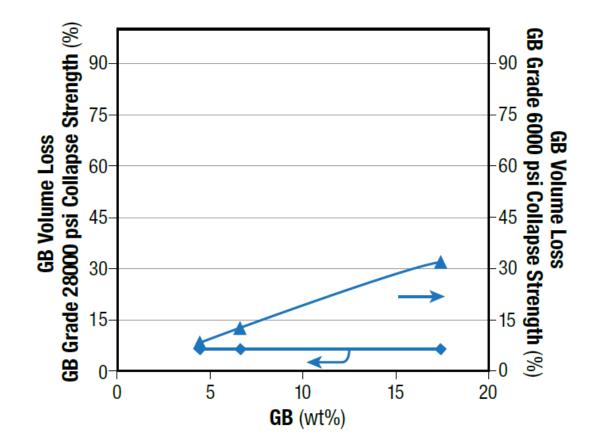
Parameters that are influential in HGM Survival During Compounding -Effect of Polymer Viscosity

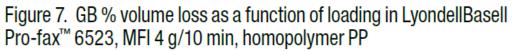


HGM(6000 psi collapse strength) % volume loss in polypropylene as a function of melt flow index (MFI). LyondellBasell Pro-fax[™] 6523. MFI (230°C/2.16 kg): 4 g/10 min and LyondellBasell Profax[™] SG899 MFI (230°C/2.16 kg): 30 g/10 min.



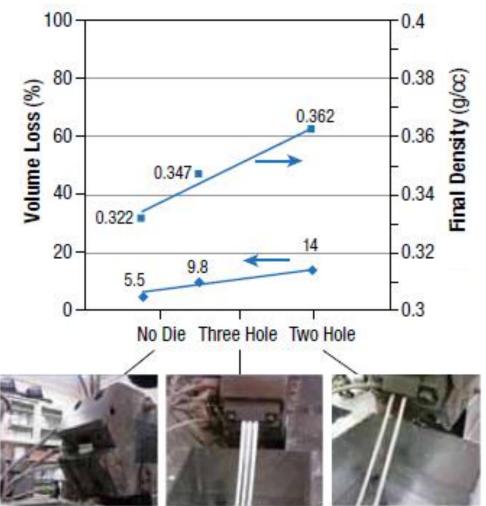
Parameters that are influential in HGM Survival During Compounding- Effect of HGM Concentration







Parameters that are influential in HGM Survival During Compounding Effect of Back Pressure





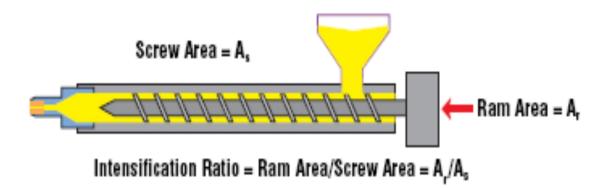
Summary of Important Things to Consider During Compounding

- 1. Twin screw co-rotating intermeshing extruders
- 2. Add HGMs into an already molten polymer at a downstream port via a side or top feeder (side feeder is preferred).
- A side feeder should be fed via a supply feeder. This will ensure starve feeding of bubbles into the polymer melt and allow various volume % loadings to be prepared. If the bubbles are flood fed into the hopper of a side feeder, clogging and bridging may occur.
- 4. Inlet design of the side feeder into the extruder is very important, especially if high volume percentages of glass bubbles are formulated. The screw elements in the inlet section should be of the conveying type with a very high OD/ID ratio, such as 1.75 or more.

- 5. Pre-heating of glass bubbles, although not mandatory, could help prevent rapid temperature decrease of the polymer melt, which could cause rapid increase in viscosity.
- 6. After the glass bubbles are added into the molten polymer, they should be conveyed via standard conveying screw elements for a while before entering distributive block sections (if any need to be used).
- 7. Minimal back pressure is preferred during compounding with glass bubbles. In this respect, a die design that creates low back pressure is important. Likewise, screens with too large mesh sizes should be avoided.
- 8. An underwater pelletizer is the preferred method of pelletizing
- If possible, resin parameters should be considered to prevent breakage – lower viscosity, higher MFI resins are preferred as well as materials that are softer and more elastic.



Injection Molding Considerations



- Maintain Low Back pressure
- •Set low screw rotation speed (RPM) and injection rate
- Maintain injection pressure x intensification ratio < Isostatic Crush Strength</p>
- General-purpose injection screw



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Benefits of HOIOW Glass Microspheres

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The Power to Do More

- Reduced density
- Increased flexural and tensile modulus
- Since they are isotropic with an aspect ratio of 1 (minimal surface area) and do not orient themselves or cause orientation to the polymer molecules, injection molded parts have uniform shrinkage leading to improved warpage and dimensional stability
- Since they take up resin volume and in some cases provide nucleation sites for crystalline polymers, increased productivity can be achieved for injection molded or thick extruded profiles due to fast cooling cycles.
- Decreased CLTEs, decreased thermal conductivity
- Increased bulk, compressive modulus, increased hardness and scratch resistance, increased HDT



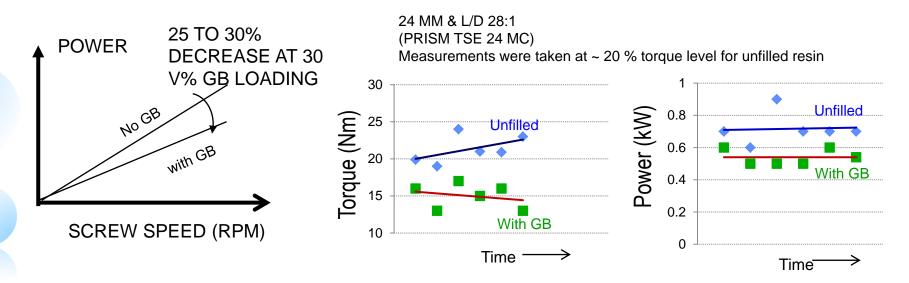


Reduced Power Requirement During Compounding

POWER = TORQUE X 2π SCREW SPEED (RPM)

Achieve higher volumetric throughput with glass bubbles or reduce torque and hence power requirements for a given volumetric throughput

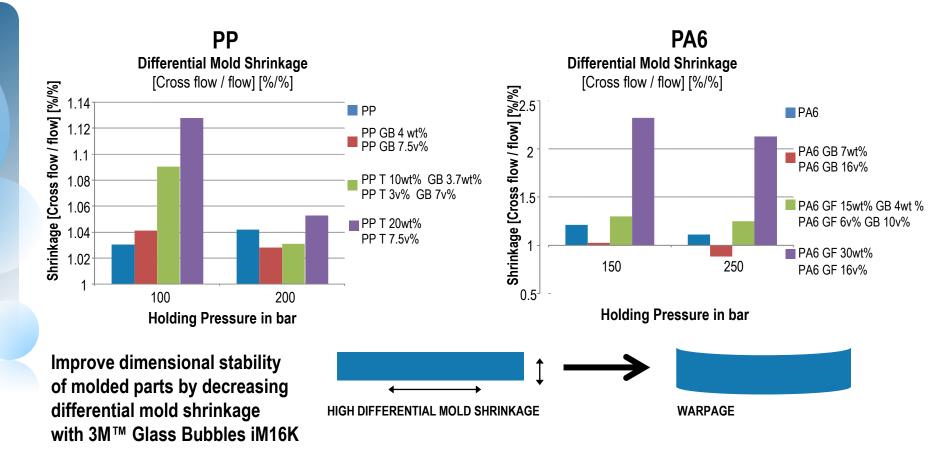
EXAMPLE : HOMOPOLYMER PP WITH AND WITHOUT GB AT 30 VOL%





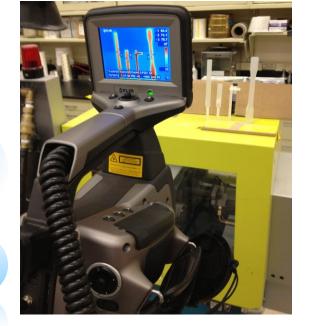
Dimensional Stability in PP and PA6

Independent Study by SKZ Institute, Germany According to DIN EN ISO 294-4





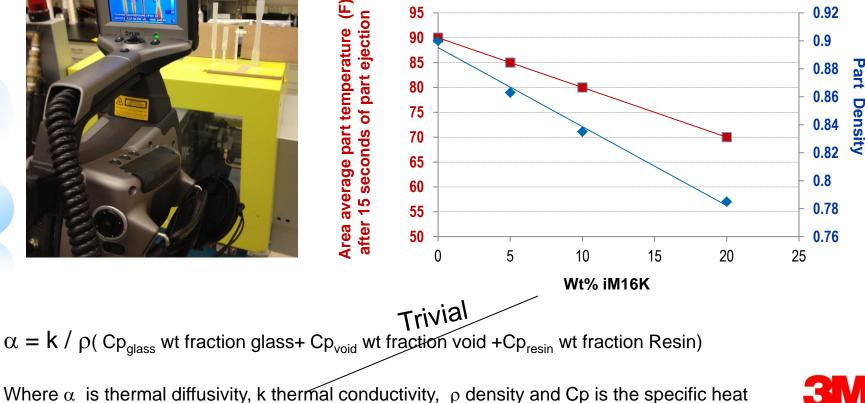
Effect of Glass Bubbles on Injection Molding Part Cooling Rate



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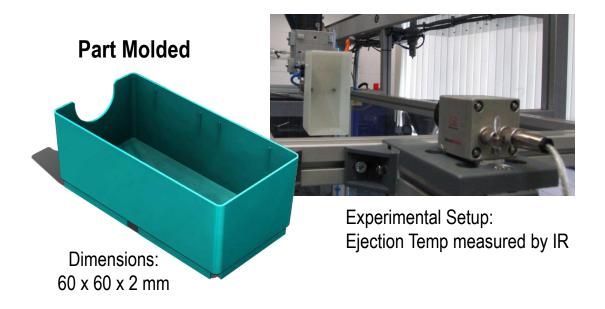
39

Injection mold temp: 135 F Holding Pressure: 3000 Psi Mold: ASTM Mold Base Polymer : PP Homopolymer



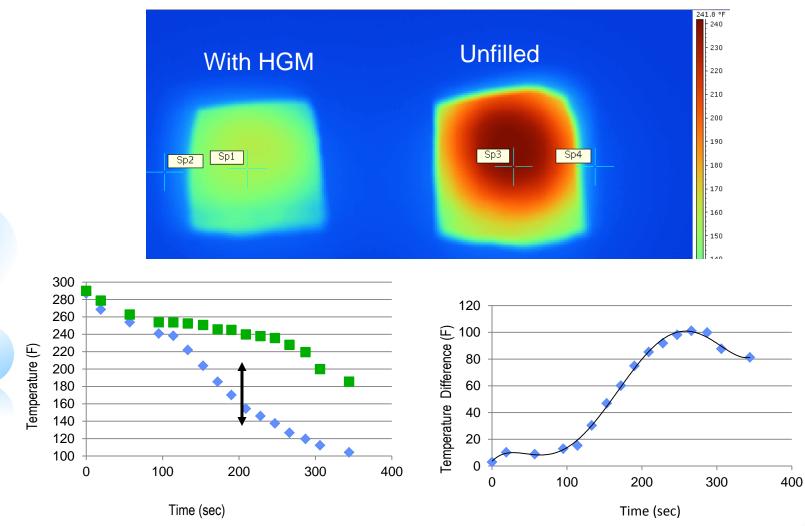
Independent Study by SKZ Institute, Germany

Material	Total Cycle Time t _G [s]	Cycle Time Reduction in [%]
PA6	40.2	_
PA6 GB-16 v%	35.2	12
PA6 GF 15–6 v% GB–10 v%	38.2	5





Effects of HGMs on Cooling from the Melt

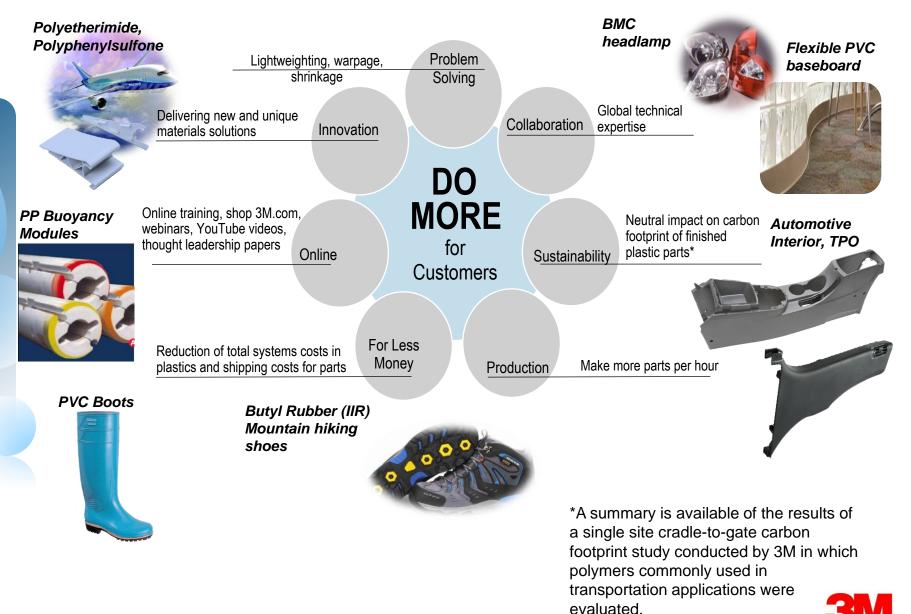




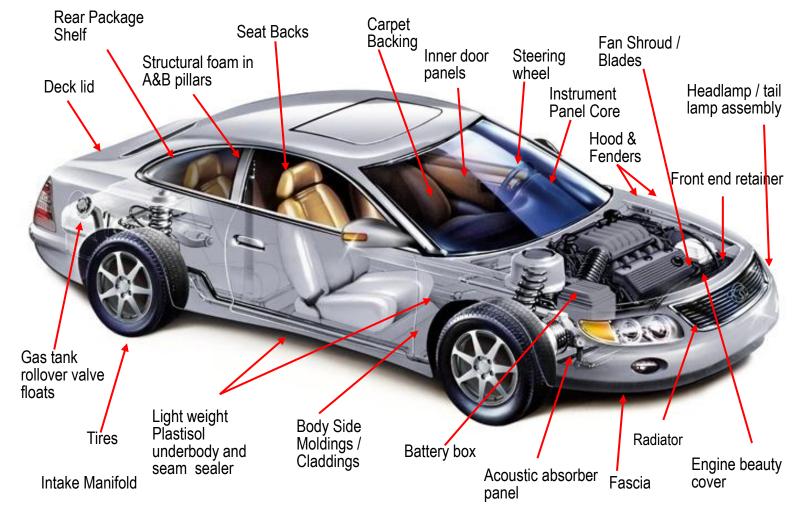
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Application Examples

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Industrial Business Group Hollow Glass Microspheres - Current & Potential Automotive Applications





Examples of Commercial Glass Bubbles Applied Parts





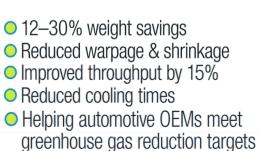
HANIL E-HWA CO., LTD





Visteon

Visteon Interiors Korea Ltd.



Photos provided by Magna, Hyundai Engineering Plastics and Visteon with customer claims as portrayed at NPE 2012. Photo provided by Hanil e-Hwa with customer claims in 2010.



Injection Molded Parts

Materials used: Talc Filled PC/ABS Deck Lid

Enabling Features:

- Reduced weight
 - Control 5.5 lbs
- ■7.5 wt. % GBs 5.0 lbs
- Class A Paint-able Surface
- Same Process Conditions





Fuel Floats

Materials used:

Nylon 6,6

Enabling Features:

- Reduced weight
- 33 Wt. % S60HS
- Final density of 0.90 g/cc
- Allowed use of existing tooling
- Material specification



The following ASTM callout has been developed for GB1430-N :

ASTM D 4000 PA0120KD044PM018UM034YI095Z01Z02Z03Z04

Callout	ISO Method	Unit	Value
PA0120 (heat stabilized nylon 66			· ·
KD044 (tensile strength)	ISO 527	Mpa	44 min.
PM018 (Izod impact)	ISO 180	kJ/m2	1.8 min.
UM034 (flexural modulus)	ISO 178	Mpa	3400 min.
YI095 (HDT @ 1.8 Mpa. flat)	ISO 75	deg. C	95 min.
Z01= (filler hollow glass bubbles	3)		
Z02=(ash)	ISO 3451	%	33 +/- 4
Z03 = (density)	ISO 1183	g/cm3	.90 +/02
Z04= (viscosity)	ISO 307	%	1.45-1.85



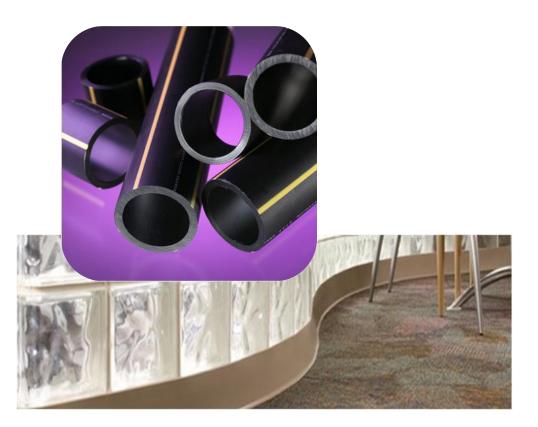
Extruded Profiles

Materials Used:

PVC or Filled PVC

Enabling Features:

- Increased throughput due to lower density/reduced cooling time (10 – 15%)
- Reduced weight
- Reduced warpage
- Improved feeding
- Meets flammability requirements







5kg weight savings per aircraft
1000 liters fuel savings/year
Reduction in carbon emissions





Low-density polymer systems specifically for the aircraft industry have been developed using 3M[™] Glass Bubbles in high temperature high performance polymers such as Polyether imide (PEI) and polyphenylsulfone (PPSU).

Photo provided by REHAU as portrayed at NPE 2012.





Photo provided by Kohshin Rubber Co., Ltd. as portrayed at NPE 2012.



Glass Bubbles in Shoe Soles

- FEATURE
 - KOLON SPORT ™ FEATHER
 - 3M[™] Performance Additives iM30K incorporated
 - Floats in the water
 - Work with research institute (KIFLT)
- BENEFIT
 - Less weight and comfort
 - Less fatigue

- ADVANTAGE
 - Weight reduced (20%)
 - − Control 1.18g/cc \rightarrow under 1.0g/cc at 11% iM30K
 - Improved dimensional stability
 - Water & chemical resistant





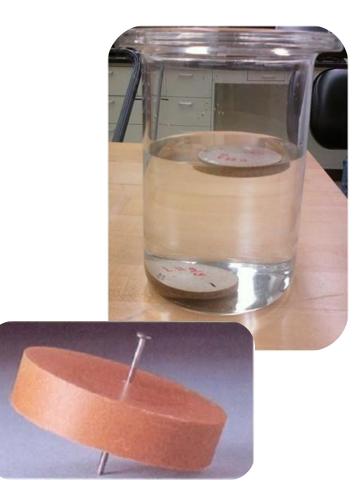
Polymer Wood Composites

Materials used:

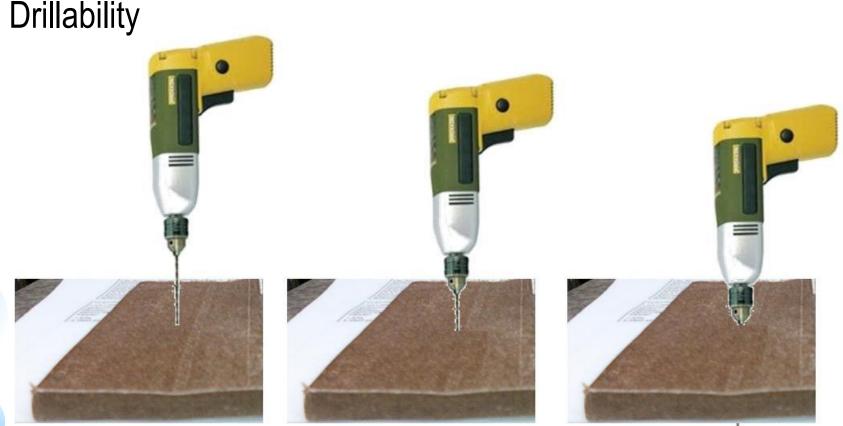
Virgin and Recycled HDPE, PVC

Enabling Features:

- Reduced Weight (5 15%)
- Reduced Cooling Time
- Improved Nail-ability
- Reduced Flammability





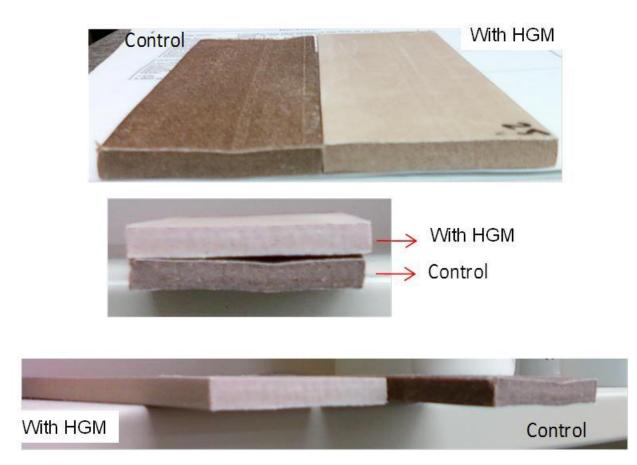


Pressure at the wood-drill bit contact point by dividing the weight of the drill by the cross sectional area of the $\frac{1}{4}$ " drill bit. 1800 grams drill weight applies a pressure of ~80 psi at the contact point.

75 SECONDS VS 20 SECONDS WITH GLASS BUBBLES (18 wt% GB)



Improved Dimensional Stability





Reduced Differential Weighting

Materials used:

Polypropylene

Enabling Features:

- Reduced/differential weighting
- Improved buoyancy
- Even wear
- Improved material flowability in mold
- Allowed use of existing tooling





Pressure-resistant thermal insulation and buoyancy

Materials used:

PP, PU, Epoxy, Silicon

Enabling Features:

- Reduced weight
- Density change
- Thermal conductivity
- High loading of GBs



Glass Bubble	W/m K	Btu in/h ft2 F
K1	0.047	0.327
K15	0.055	0.38
K20	0.07	0.486
S22	0.076	0.529
K25	0.085	0.593
S32	0.108	0.746
S35	0.117	0.813
K37	0.124	0.858
S38/ S38HS/ S38XHS	0.127	0.88
K46	0.153	1.062
S60/ S60HS	0.2	1.39





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Conclusion

Hollow Glass Microspheres can reduce density of materials while providing significant processing benefits with improved properties.

Smart formulation is key in attaining an acceptable balance of weight and final properties.



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Thank you!



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